

2nd In-class Exam, Apr. 13

Take home exam (final exam) Apr. 27, due May 6.

Reading:

6.5 Global leakage

10.3 Toroidal particle trapping

P158 Safety factor q

4.5 ICF (Review)

9.3-9.5 Magnetic Mirror

(Banana orbits \rightarrow neoclassical D, where $D \sim \frac{r_g}{\zeta_s}$ instead of classical $D \sim \frac{r_g}{\zeta_s}$)

for subsequent comparison to Tokamaks

HOMEWORK 8

Homework = 30% of exam, turn in Apr. 13.

Note change
4/6/10

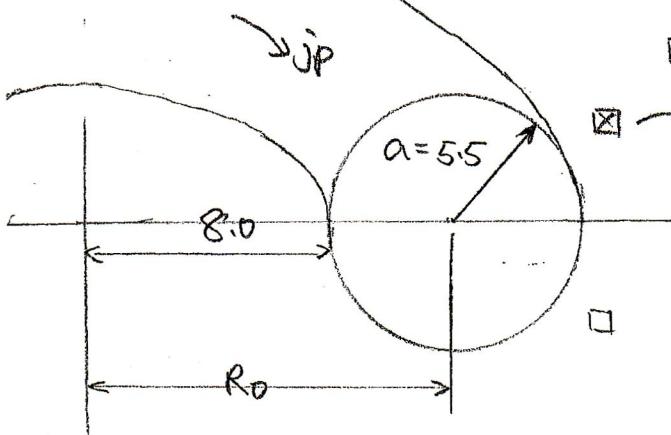
~~ITER~~ (see ITER internal website) <http://www.iter.org/default.aspx>

1) What is the goal of ITER? (Hint: Engineering and Physics goal) What needs to be done then to make it a power plant?

(Physics: , such as the energy balance. Eng: Blanket, etc.)

2) Make a table of specs of ITER: R_0 , a , B_T , $B_\theta(a)$, P_{in} (plasma & auxiliary), Fueling rate, Fusion power level P_f . Assume an equivalent circle cross section as shown below.

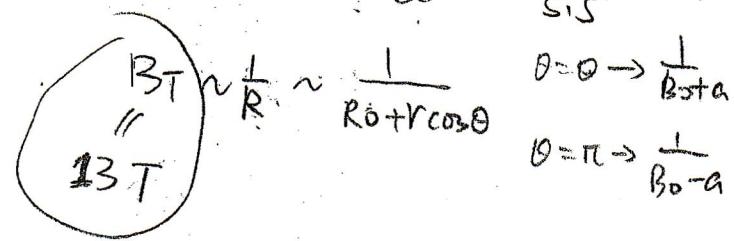
(In "The Machine" drawdown menu, a lot of info is provided.)



$$B_T \sim \frac{1}{R}, a = 5.5 \text{ m}$$

$$R_0 = (8 + 5.5) \text{ m}$$

$$A_S = \frac{R_0}{a} = \frac{8 + 5.5}{5.5}$$

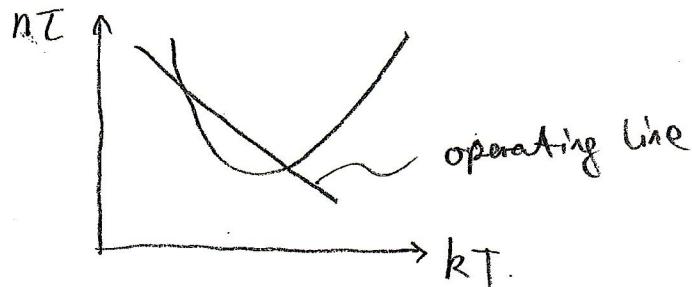


(2)

- 3). Plot nT_{ig} vs. kT for an ITER plasma.

(Hint: p132-133). To get rid of N , $N = \frac{\beta B_0^2}{4\mu kT}$

Assume $\beta = 5\%$ max.

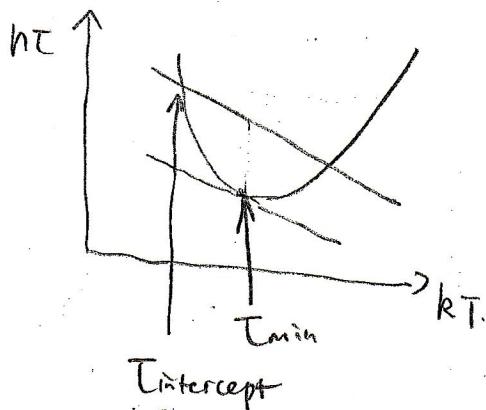


- 4) Add ITER operating line to graph, i.e. nT_{ITER} vs. kT .

$$\left(\text{classical } D_{\perp} \sim \frac{r_g^2}{\tau} \sim \text{constant. } \frac{1}{B^2 \sqrt{kT}} \right)$$

$$nT = K n_0 B_0^2 \sqrt{kT}$$

- 5). Calculate confinement time margin $\equiv \frac{T_{\text{min}}}{T_{\text{intercept we calculate}}}$



≈ 10³

(3)

HW #8 [continued] (Plus discussion)

4/6/10

- 6) Wall Loading: Plasma and Radiation heating present wall cooling challenge. Keep $< \text{few MW/m}^2$. Neutron material damage sets limit on neutron "power" loading (actually power associated with neutrons passing through wall) of $\gtrsim 1 \text{ MW/m}^2$.

Assume ITER uses 50/50 DT and operates at the $n_e - h_T$ intercept you found in 5) (or if not found, used min $n_e - h_T$ on energy balance curve of 3)); calculate the corresponding "heating and neutron" wall loading in MW/m^2 . Do they fall in allowed limits. If not, suggest how to change the design to adjust the loadings.

- 7) Ash issue: The α particles from fusion are generally contained in the plasma. They provided the needed "ignition" heating but as they slow down & thermalize, they become a useless diluent or "ash" in the plasma; i.e., $N_{\text{total}} = N_p + N_T + N_{\alpha}^{\text{ash}}$. Assume that the confinement times for all ions are equal ($\tau_p = \tau_T = \tau_{\alpha}$). Find the equilibrium % of ash in the ITER plasma. (Hint: use $\frac{dN_{\alpha}}{dt} = S_{\alpha} - L_{\alpha} = 0$)

(4)

Evaluate the resulting change in fusion power and radiation emission in ITER.

Could this cause ITER to fall below ignition (= "sub-ignited").

Discuss your answer - include discussion of the possibility that $\bar{\tau}_\alpha > \bar{\tau}_{DT}$ -- indicate a rough limit on the allowed $\bar{\tau}_\alpha$.

8) Ohmic heating of plasma.

Ohmic heating comes from the plasma current, I_p , which also creates B_θ . A first approximation of the plasma resistivity η is:

$$\eta \approx \frac{9.6 \times 10^{-6}}{(kT)^{3/2}} \text{ ohm-cm} \quad (\text{Ref. } G+PP TOB3)$$

where $\eta \equiv E / j_p$: $E = \text{electric field around torus}$ [note; $E = I_p R_2 = \frac{I_p (B_0 A)}{2\pi a}$]

$$\left[\frac{I_p (B_0 A)}{2\pi a} = j_p \eta \right].$$

We can find I_p from $B_\theta(a) = \frac{\mu I_p}{2\pi a}$

and requiring that $q(a) \geq 2.5$

since $q \equiv \frac{1}{A} \frac{B_I}{B_\theta}$, in ITER

Evaluate the ohmic heating power: $P_\Omega \text{ MW/m}^3$

Compute the % of the total plasma heating that is due to ohmic power when the ITER plasma is ignited. Is the term "ignited" still applicable?

(5)

For our text, pp 161-62, we see that E comes from transformer action, i.e. dV/dt . Evaluate the flux rate $d\Phi/dt$ needed for ITER. Does this agree with data from the web site? How would you prevent the vacuum vessel wall from shorting out E ? [note E is $E_{toroidal}$ and wall materials are generally conductors]. Does your suggestion agree with the web site? [if nothing is said about these pts on web, not that]

- ⑦ The vertical field B_y prevents up-down motion of the plasma. Field ordering is $B_T > B_\theta \gg B_r$. Make a sketch showing the location of the vertical field coils in an ITER like device. Estimate the strength (Tesla) of B_y . Could B_y affect particle orbits in the plasma? - discuss your answer.

- ⑩ Consider the divertor on ITER. Is a single or double poloidal divertor used on ITER (see ^{our} web site)? Assume 3/2's of the plasma leakage power enters the divertor ($1/2$ goes to wall). Estimate the heat load assuming a divertor "dump" plate is ≈ 0.3 a high. Does this

(6)

fit into loading limits stated in 6)? If not suggest how to modify the design to handle the load.

The $\frac{1}{3}$ of the plasma flux going to the wall causes sputtering. Assume a sputtering rate of 0.01 atoms Fe per cm hitting. Assume $\tau_{Fe} = \tau_{D^2}$. What would the concentration (N_p) of the Fe in the plasma be? How much would the radiation power be changed by sputtering?

(11) Extra credit: Estimate the fueling rate required for ITER. Estimate the power required to heating injected ions up to the plasma temperature, assuming they begin at room temperature ≈ 0.063 eV.

[This; note $\frac{dN_p}{dT} = \frac{N_p}{T}$. also]

$$P_{heat\text{ or }} \approx \frac{N_p}{T} (kT - kT_{room})$$

How does ITER inject (and heat) fuel? Do your estimates agree with the web site? - discuss.

(12) Extra credit #2: Find a recent "ITER scaling law" agreed to by the ITER Council. Compare it to our classical one using plots of the two on N_p vs kT , graph. Discuss differences.